

## The effects of the ovarian cycle and pregnancy on uterine vascular impedance and uterine artery mechanics

Benjamin J. Sprague<sup>a,b</sup>, Terrance M. Phernetton<sup>b</sup>, Ronald R. Magness<sup>b,c,d</sup>, Naomi C. Chesler<sup>a,\*</sup>

<sup>a</sup> Department of Biomedical Engineering, University of Wisconsin, Madison, WI, USA

<sup>b</sup> Department of Ob/Gyn Perinatal Research Laboratories, University of Wisconsin, Madison, WI, USA

<sup>c</sup> Department of Animal Sciences, University of Wisconsin, Madison, WI, USA

<sup>d</sup> Department of Pediatrics, University of Wisconsin, Madison, WI, USA

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### ABSTRACT

**Objectives:** Uterine vascular resistance (UVR) is the ratio of systemic mean arterial pressure to mean uterine blood flow and is sensitive to changes in small arteries and arterioles. However, it provides little or no insight into changes in large, conduit arteries. Fluctuations in estrogen (E2) and progesterone (P4) levels during the ovarian cycle are thought to cause uterine resistance artery vasodilation; the effects on large arteries are unknown. Herein, our objective was to use the uterine vascular impedance, which is sensitive to changes in small and large arteries, to determine the effects of the ovarian cycle and pregnancy on the entire uterine vasculature.

**Study design:** Uterine vascular perfusion pressure and flow rate were recorded simultaneously in anesthetized sheep in the nonpregnant (NP) luteal (NP-L,  $n = 6$ ) and follicular (NP-F,  $n = 7$ ) phases and in late pregnancy (CP,  $n = 10$ ). Impedance and metrics of impedance (input impedance  $Z_0$ , index of wave reflection  $R_w$ , characteristic impedance  $Z_c$ ) were calculated. E2 and P4 levels were measured from jugular vein blood samples. Finally, from pressure-diameter tests post-mortem, large uterine artery circumferential elastic modulus ( $E_{Circ}$ ) was measured. Significant differences were evaluated by two-way ANOVA or Student's *t*-test.

**Results:** As expected, E2:P4 was higher in the NP-F group compared to the NP-L group ( $p < 0.05$ ). Also as expected, UVR and  $Z_0$  decreased in the follicular phase compared to the luteal ( $p < 0.05$ ), but  $R_w$ ,  $Z_c$ , and  $E_{Circ}$  were unaltered. Pregnancy not only substantially decreased UVR (and  $Z_0$ ) ( $p < 0.00001$ ) but also decreased  $Z_c$  ( $p < 0.001$ ),  $R_w$  ( $p < 0.0001$ ),  $E_{Circ}$  ( $p < 0.01$ ), and pulse wave velocity ( $p < 0.0001$ ).

**Conclusions:** The E2:P4 ratio mediates resistance artery vasodilatation in nonpregnant states, but has no effect on conduit artery size or stiffness. In contrast, pregnancy causes dramatic vasodilation and remodeling, including substantial reductions in conduit artery stiffness and increases in conduit artery size, which affect pulsatile uterine hemodynamics.

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## 1. Introduction

In contrast to the vascular resistance, which measures the opposition to mean or steady flow in a vascular network, vascular impedance measures the opposition to pulsatile flow. Since nearly all blood flow in the body is pulsatile in nature, impedance reflects the true work required to perfuse a vascular bed. Also, since the mean flow is a component of any pulsatile flow, resistance can be directly obtained from the frequency-dependent impedance

spectrum. Indeed, 0 Hz impedance measured *in vivo* is equivalent to the vascular resistance distal to the point-of-measure. Moreover, impedance yields other useful metrics of circulatory function such as the characteristic impedance ( $Z_c$ ), which provides insight into arterial size and stiffness, and index of wave reflection ( $R_w$ ), which reflects the effects of taper, branches and changes in arterial stiffness on pressure and flow waveforms [1]. Finally, impedance inherently contains more information than resistance, which may be useful in diagnosing vascular bed abnormalities such as may occur with infertility or in preeclampsia with and without intrauterine growth retardation. However, the changes in uterine vascular impedance that occur during the ovarian cycle and with healthy pregnancies have not been reported.

The ovarian cycle is characterized by fluctuations in the sex hormones estrogen (E2) and progesterone (P4) [1]. The luteal

\* Corresponding author at: Department of Biomedical Engineering, University of Wisconsin at Madison, 2146 Engineering Centers Building, 1550 Engineering Drive, Madison, WI 53706-1609, USA. Tel.: +1 608 265 8920; fax: +1 608 265 9239.

E-mail address: [chesler@engr.wisc.edu](mailto:chesler@engr.wisc.edu) (N.C. Chesler).

phase is a time of relatively low E2 and high P4 whereas the follicular phase, in which the uterus is readied for implantation, is a time of higher E2 and lower P4 [2–4]. Increased E2:P4 is known to increase mean blood flow to many vascular beds, especially the uterus [2,5–16]. Local, exogenous treatment with E2 can also increase blood flow to the uterine vascular bed [9,12,16]. Since blood pressure does not change significantly over the ovarian cycle, these increases in blood flow are enabled by a drop in UVR, presumably by arteriolar vasodilation. Changes in large artery size and stiffness over the ovarian cycle have not been investigated to our knowledge. Furthermore, changes in pulsatile uterine hemodynamics over the ovarian cycle, which would be a consequence of altered large artery structure and function, have not been reported.

In healthy pregnancies, uterine blood flow increases by 20–50-fold with little to no change in perfusion pressure [10,14,17–19]; thus, uterine vascular resistance (UVR) typically decreases 20–50-fold. This dramatic drop is enabled in part by the physiological transformation of resistance-sized arteries into the uteroplacental bed [20–24] and also by large uterine artery remodeling [20–25]. In particular, in healthy pregnancies large uterine arteries grow in diameter nearly 2-fold and become less stiff [20–26]. Nevertheless, changes in pulsatile uterine hemodynamics with pregnancy are not typically reported.

The goals of this study were to determine the effects of the ovine ovarian cycle and healthy pregnancy on uterine vascular impedance, and the dependence of impedance changes on large, conduit uterine artery structure and function changes. We hypothesized that UVR and input impedance would decrease during the follicular phase in response to the increased E2:P4 ratio, but that changes in conduit arteries would be minimal. In addition, we hypothesized that pregnancy would result in dramatically decreased UVR (by 20–50-fold) as well as increased large artery diameter and decreased large artery stiffness, characteristic impedance, wave reflections and pulse wave velocity (PWV). Finally, we investigated the effects of the ovarian cycle and healthy pregnancy on the clinically used blood flow indices systolic to diastolic ratio (S/D), resistivity index (RI) and pulsatility index (PI).

## 2. Materials and methods

### 2.1. Animal preparation

Procedures for animal handling and protocols for experimental procedures were approved by the University of Wisconsin-Madison Research and Animal Care and Use Committees of both the Medical School and the College of Agriculture and Life Sciences. This study contained three groups of multiparous female sheep of mixed western breeds: two nonpregnant (NP) groups synchronized to different phases of the ovarian cycle and one late-gestation, pregnant group. The NP animals ( $n = 13$ ) were experimentally synchronized to be sacrificed during two distinct and controlled points of the ovarian cycle, i.e. the late follicular phase during the periovulatory period (NP-F,  $n = 7$ ) and the late luteal phase 10–11 days post-ovulation (NP-L,  $n = 6$ ), as previously described [2]. Briefly, controlled internal drug-releasing devices (CIDRs) were placed vaginally to deliver luteal phase levels of progesterone for 9–11 days. Upon removing the CIDR, injections of prostaglandin F2 alpha (7.5 mg Lutalyse) and pregnant mare serum gonadotropin (PMSG) (500 IU) were given IM. The late follicular/periovulatory and luteal phases were defined as 48 h and 12–13 days post-CIDR removal and injections, respectively. Pregnant animals were studied as a positive control of (expected) significant changes in large artery mechanics. The control pregnant group (CP,  $n = 10$ ) was studied at 120–130 days gestation. The natural gestation length for sheep is 145–147 days.

### 2.2. Hemodynamic measurements

During non-survival surgery just prior to sacrifice, animals were anesthetized with pentobarbital sodium (Nembutal; 50 mg/ml) via a jugular vein catheter. Then, in the supine position, uterine artery pressure was measured with a fluid filled catheter inserted via cannulation of the saphenous branch of the femoral artery and advanced to the level of the internal iliac, near the origin of the uterine artery [11,15]. Heart rate (HR) was also measured from this pressure waveform. Following a midventral incision, the primary uterine arteries supplying each horn of the uterus in the mesometrium were identified and isolated. Uterine blood flow in one of these arteries (i.e., unilateral) was measured using a cuff-type ultrasonic flow probe. Depending on the size of the artery, 3 or 6 mm ultrasound probes (3RS and 6RS probes, Transonic Systems Inc., Ithaca, NY) were used. Pressure and flow measurements were sampled simultaneously at 120 Hz using WinDaq Pro Data Acquisition software (DATAQ Instruments, Akron, OH) [11,15].

### 2.3. Hemodynamic analyses

Pressure and flow waveforms for ten sequential cardiac cycles were isolated and independently analyzed. UVR was calculated as mean systemic arterial pressure ( $P_{\text{Mean}}$ ) divided by mean uterine blood flow ( $Q_{\text{Mean}}$ ):

$$\text{UVR} = \frac{P_{\text{Mean}}}{Q_{\text{Mean}}} \quad (1)$$

This equation is equivalent to the more traditional definition of resistance as mean pressure difference across a vascular bed divided by mean flow through the vascular bed if the downstream (uterine venous) pressure is close to zero or constant over the ovarian cycle and with pregnancy, which is typically assumed for the uterine venous bed ( $\sim 1$ – $2$  mmHg).

To calculate input impedance in the frequency domain, each cardiac cycle underwent processing to eliminate signal noise that included applying a Hann window and zero-padding (MATLAB, The MathWorks Inc., Natick, MA). These processed waveforms were then resolved into their frequency components using a discrete fast Fourier transform function (MATLAB) and their ratio taken at all harmonics of the heart rate as previously described [27–29]. Here we present only impedance magnitude because the distance between the sites of pressure and flow measurement made the impedance phase calculation an unreliable measure of pressure–flow lag without additional calibration studies. Furthermore, the impedance phase contains less information than the impedance magnitude [30].

Several metrics of the input impedance were calculated. The input resistance ( $Z_0$ ) was calculated as the input impedance magnitude at 0 Hz.

$$Z_0 = Z(f = 0 \text{ Hz}) \quad (2)$$

Characteristic impedance,  $Z_C$ , was calculated as the average impedance magnitude for all frequencies above the first minimum of each impedance spectrum [28].

$$Z_C = \langle Z(f > f_{\min(Z)}) \rangle \quad (3)$$

Finally, the index of wave reflection,  $R_W$ , was computed as in [30]:

$$R_W = \frac{Z_0 - Z_C}{Z_0 + Z_C} \quad (4)$$

Coefficients of variation for these impedance metrics over the ten cycles of data collected for each animal were less than 8%; the average value was used for each animal.

Clinically used indices of blood flow, S/D, RI and PI, were calculated using the peak systolic flow ( $Q_{Sys}$ ), end-diastolic flow ( $Q_{Dia}$ ), and mean uterine blood flow  $Q_{Mean}$  as in [31]:

$$\frac{S}{D} = \frac{Q_{Sys}}{Q_{Dia}}$$

$$RI = \frac{Q_{Sys} - Q_{Dia}}{Q_{Sys}} \quad (4)$$

$$PI = \frac{Q_{Sys} - Q_{Dia}}{Q_{Mean}}$$

#### 2.4. Estrogen and progesterone measurements and analyses

Jugular vein blood samples were collected into vials containing ethylene diamine tetraacetic acid (EDTA) and centrifuged for isolation of blood plasma. Blood plasma was stored frozen ( $-20^{\circ}\text{C}$ ) until 17- $\beta$  estradiol (E2) and progesterone (P4) hormone levels were analyzed. To analyze E2, plasma (400  $\mu\text{l}$ ) was extracted with diethyl ether and concentrations of E2 were evaluated by RIA as previously reported [2,3,32]. Plasma P4 was analyzed using the commercial Coat-A-Count RIA kit from Diagnostic Products Corporation (DPC, Los Angeles, CA). All samples were analyzed in duplicate and in a single assay (intra-assay percent relative standard deviations were 3.9% for E2 and 11.2% for P4).

#### 2.5. Large uterine artery mechanical measurements

After hemodynamic data and blood samples were obtained, animals were euthanized and the uterus was removed. The uterine arterial tree was dissected from each (right and left) uterine horn. In each excised arterial tree, one primary, two secondary and at least four tertiary (third generation) arteries were obtained intact. One secondary artery from each horn (right and left) was randomly selected for mechanical testing and placed in a cold ( $4^{\circ}\text{C}$ )  $\text{Ca}^{2+}$ -free, KREBS + HEPES solution (composition (mM): NaCl 144; KCl 5.9;  $\text{MgCl}_2$  1.2; glucose 11; Hepes 10; pH 7.4) with 0.1 mM EGTA (Ethylene glycol-bis-(2-aminoethyl)-N,N,N',N'-tetraacetic acid) to ensure fully relaxed smooth muscle cells.

For mechanical testing, one end of each artery was cannulated with polyvinyl tubing with an outer diameter between 1.5 and 2.5 mm. The  $\text{Ca}^{2+}$ -free, KREBS + HEPES solution with 0.1 mM EGTA was heated to  $37^{\circ}\text{C}$  and used as both perfusate and superfusate. The other end and all side branches of the artery were tied off. No initial stretch was imposed; the artery was provided no anchoring in the longitudinal direction but allowed to expand freely. After an initial equilibration period (30 min), intraluminal pressure was increased from 0 to 120 mmHg in a stair-step manner in 10 mmHg increments. The isolated artery was digitally photographed at  $12\times$  magnification to obtain the pressure-dependent outer diameter ( $OD_p$ ) and axial length ( $L_p$ ) via externally visible landmarks on the artery segments in each loaded state. The OD and length measurements taken at zero transmural pressure were used as a reference state ( $OD_0$  and  $L_0$ , respectively).

Following the stair-step pressurization tests, arteries were fixed at approximate *in vivo* pressure (85–95 mmHg) [10–12,15,33,34] with 4% formalin solution for at least 2 h. Outer diameter and length were measured post-fixation ( $OD_f$  and  $L_f$ , respectively). To measure inner diameter and wall thickness post-fixation at the *in vivo* pressure ( $ID_f$  and  $WT_f$ , respectively), three to four rings were cut from the fixed tissue in 0.25–0.35 mm lengths. These sections were then digitally photographed in cross-section. Inner and outer circumferences were measured for each ring and used to calculate inner and outer diameter, respectively, assuming circular cross-

sections ( $ID_f$  and  $OD_{f,ring}$ , respectively).  $WT_f$  was calculated as follows:

$$WT_f = \frac{OD_{f,ring} - ID_f}{2} \quad (6)$$

The agreement between  $OD_f$  and  $OD_{f,ring}$  served as a useful check on the measurement integrity.

Image analysis software (MetaVue, Molecular Devices, Downingtown, PA) calibrated to scales on each image were used to make all measurements from digital photographs.

#### 2.6. Large uterine artery mechanical analyses

In order to calculate uterine artery elastic modulus, circumferential stress and strain at each pressure step were calculated. First, circumferential Green strain ( $\epsilon_{Circ}$ ) was calculated based on stretch from the zero pressure state:

$$\lambda_{Circ} = \frac{OD_p}{OD_0} \quad \epsilon_{Circ} = \frac{1}{2}(\lambda_{Circ}^2 - 1) \quad (7)$$

Then, inner diameter at each pressure ( $ID_p$ ) was calculated from the fixed dimensions assuming conservation of volume:

$$ID_p = \sqrt{\frac{L_f}{L_p}(OD_f^2 - ID_f^2) + OD_p^2} \quad (8)$$

Cauchy circumferential stress ( $\sigma_{Circ}$ ) at the inner wall surface was calculated using a thick-walled assumption because the ratio of  $ID_p/WT_p$  was less than 20 for most pressures:

$$\sigma_{Circ} = \frac{P(OD_p^2 + ID_p^2)}{OD_p^2 - ID_p^2} \quad (9)$$

where  $P$  is the transmural pressure at which  $OD_p$  and  $ID_p$  were measured. Finally, circumferential incremental elastic modulus ( $E_{Circ}$ ) was calculated as the slope of the circumferential stress versus circumferential strain relationship over a physiological pressure range.

Also, uterine artery PWV was approximated using the Moens–Korteweg equation for a thick-walled vessel based on the fixed dimensions:

$$c_0 = \frac{E_{Circ}(OD_f^2 - ID_f^2)}{3\rho OD_f^2} \quad (10)$$

where  $\rho$  is the density of blood ( $1.06 \text{ g/cm}^3$ ).

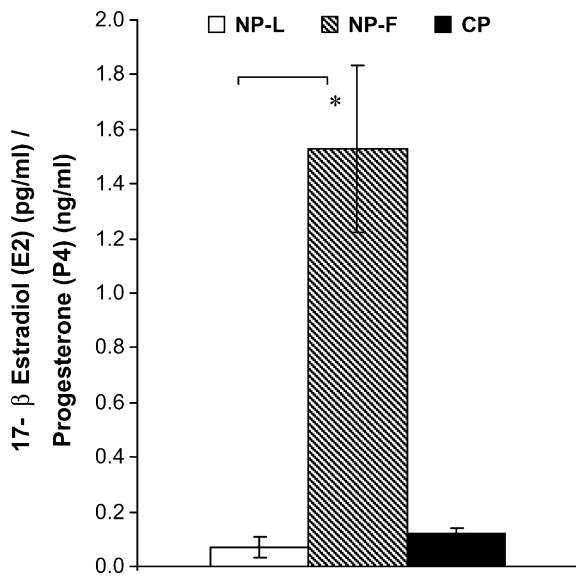
#### 2.7. Statistical analysis

All results are expressed as mean  $\pm$  S.E. Significance of the differences between the various groups was evaluated by two-way ANOVA or Student's *t*-test. The results were considered statistically significant when  $p < 0.05$ .

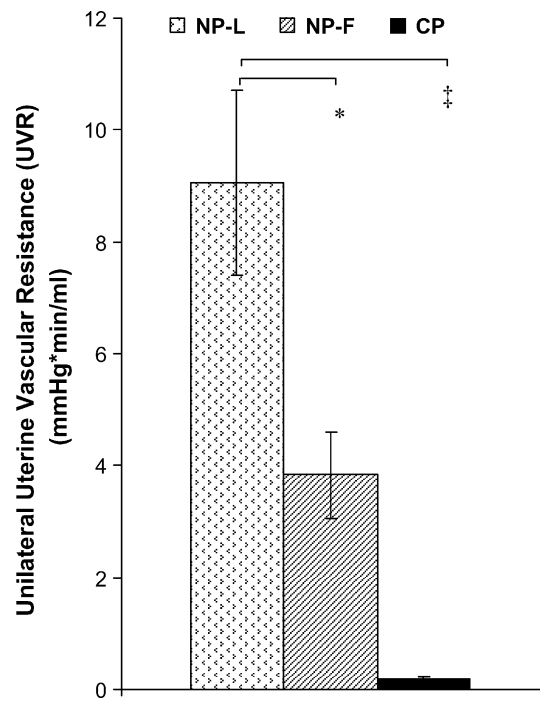
### 3. Results

#### 3.1. Estrogen and progesterone measurements and analyses

The ratio of 17- $\beta$  estradiol (E2) to progesterone (P4) in systemic plasma was higher in NP-F compared to NP-L animals ( $p < 0.05$ ), primarily as a result of very low levels of P4. NP-F animals tended to have higher levels of E2, but this difference did not reach statistical significance ( $p > 0.05$ ) because one animal showed an ovarian structure identified as a corpus hemorrhagicum that was consistent with recent ovulation, i.e. after E2 has peaked and is falling. As we have reported previously [2–4], the hormone profiles found here were consistent with the observed



**Fig. 1.** The ratio of 17-β estradiol (E2) to progesterone (P4) within plasma in jugular vein blood samples obtained from NP-L, NP-F and CP animals. Compared to NP-L, the E2:P4 ratio increased in NP-F (\**p* < 0.05). In pregnancy, elevated levels of both E2 and P4 returned the E2:P4 ratio to approximately NP-L levels. Data are means ± S.E.



**Fig. 2.** Unilateral uterine vascular resistance (UVR) of NP-L, NP-F and CP animals. UVR was computed as  $P_{Mean}$  divided by  $Q_{Mean}$  in one uterine artery (hence, unilateral). Compared to NP-L, UVR decreased by over 2-fold in NP-F (\**p* < 0.05) and over 20-fold in CP (†*p* < 0.00001). Data are means ± S.E.

size and appearance of the ovarian follicular and luteal structures in NP ewes (data not shown). In the pregnant sheep, levels of E2 and P4 were both approximately 10-fold greater than in the NP-L animals, leading to no difference between these groups in E2:P4 ratio (Fig. 1).

### 3.2. Hemodynamic measurements and analyses

As expected, blood flow increased 2-fold in NP-F animals compared to NP-L (*p* < 0.05), and increased 20-fold in CP animals compared to NP-L (*p* < 0.00001) (Table 1). No differences in measured pressures ( $P_{Mean}$ ,  $P_{Sys}$  and  $P_{Dia}$ ) or HR were observed (Table 1). Therefore, the calculated decreases in UVR in the NP-F and CP groups (Fig. 2) were solely due to increases in blood flow.

The impedance magnitude at 0 Hz,  $Z_0$ , for each group was identical to the UVR, as expected, which served as a useful check on the calculation. As noted above, the calculation of  $Z_C$  was based on the average impedance magnitude above the first minimum,  $f_{min(Z)}$  [28]; NP-F and CP animals tended to have a greater  $f_{min(Z)}$  (5.0–6.0 Hz) compared to NP-L (4.5–5.5 Hz), but the differences were not statistically significant (data not shown).  $Z_C$  decreased in CP animals compared to NP-L and NP-F (*p* < 0.001);  $Z_C$  tended to be lower in NP-F animals compared to NP-L, but the difference did not reach statistical significance (Fig. 3A). The index of wave reflection,  $R_w$ , also decreased in CP animals compared to NP-L and NP-F animals (*p* < 0.001), and was not different between NP-L and NP-F animals (Fig. 3B).

**Table 1**

Heart rate (HR), mean, systolic and diastolic blood pressure ( $P_{Mean}$ ,  $P_{Sys}$  and  $P_{Dia}$ , respectively) and mean, systolic and diastolic blood flow ( $Q_{Mean}$ ,  $Q_{Sys}$  and  $Q_{Dia}$ , respectively) for NP-L, NP-F and CP animals. HR and blood pressure did not vary between groups. Compared to NP-L animals, blood flow increased in NP-F and CP animals.

	HR (bpm)	$P_{Mean}$	$P_{Sys}$	$P_{Dia}$	$Q_{Mean}$	$Q_{Sys}$	$Q_{Dia}$
NP-L	145 ± 7.8	143 ± 21.1	170 ± 23.2	126 ± 19.1	17.5 ± 1.9	27.6 ± 2.9	10.0 ± 1.5
NP-F	136 ± 6.0	120 ± 6.5	140 ± 7.0	108 ± 6.2	38.0 ± 7.2*	60.3 ± 11.4*	20.4 ± 5.7*
CP	134 ± 4.8	138 ± 13.0	161 ± 15.1	122 ± 11.7	813 ± 73.2†	1070 ± 100†	610 ± 53.1†

Data are means ± S.E. All flow measurements were made in the primary artery of one uterine horn (i.e., unilaterally).

\* Indicates significant difference between NP-F and NP-L (*p* < 0.05).

† Indicates significant difference between CP and NP-L (*p* < 0.00001).

None of the clinically used blood flow indices were affected by the ovarian cycle. However, pregnancy substantially decreased the S/D ratio, RI and PI (*p* < 0.001) (Fig. 4).

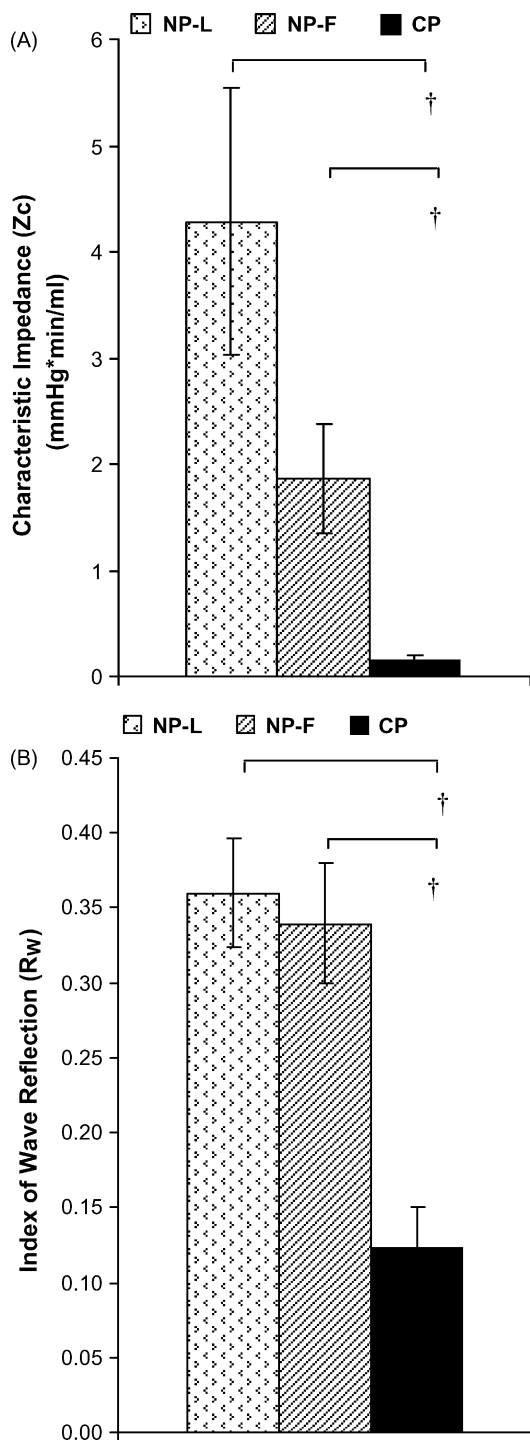
### 3.3. Large uterine artery mechanical measurements and analyses

Inner diameter and outer diameter fixed at *in vivo* pressures ( $ID_f$  and  $OD_f$ , respectively) increased in CP animals compared to NP-L and NP-F (*p* < 0.00001 for  $ID_f$  and  $OD_f$  for both groups). Wall thickness at fixed at *in vivo* pressures ( $WT_f$ ) remained unchanged throughout the ovarian cycle and with pregnancy (Table 2).  $E_{Circ}$  was not different between NP-L and NP-F groups but was significantly lower in CP animals than NP-L (*p* < 0.01) (Fig. 5). Similarly, PWV decreased in CP animals compared to NP-L (*p* < 0.0001), but was not different between NP-L and NP-F groups (Fig. 6).

## 4. Discussion

The major findings of this study are that measurements of uterine vascular impedance are able to detect significant resistance artery vasodilation mediated by the E2:P4 ratio during the ovine ovarian cycle, and do not show evidence of altered conduit artery size or stiffness via changes in metrics of impedance. In contrast,





**Fig. 3.** Metrics of uterine vascular impedance from NP-L, NP-F and CP animals. (A) Characteristic impedance ( $Z_c$ ) decreased in CP animals compared to NP-L and NP-F ( $^{\dagger}p < 0.001$ ); (B)  $R_w$  also decreased in CP compared to NP-L and NP-F animals ( $^{\dagger}p < 0.001$ ). Data are means  $\pm$  S.E.

uterine vascular impedance metrics  $Z_0$  (equivalent to UVR),  $Z_c$  and  $R_w$  are all significantly affected by normal pregnancy, as are conduit artery size, elastic modulus and pulse wave velocity as well as clinically used blood flow indices. Overall, these results demonstrate that uterine vascular impedance is a useful tool for detecting changes, and possibly abnormalities, in conduit and resistance artery structure and function over the ovarian cycle and with pregnancy.

#### 4.1. Systemic levels of estrogen and progesterone

The ratio of E2 to P4 previously has been shown to increase dramatically during the follicular phase of the ovine ovarian cycle [2,3,7,35]. In addition, E2 and P4 levels have been shown to increase several-fold during pregnancy and maintain an E2:P4 ratio equivalent to the luteal phase of the ovarian cycle [2,3,7,35,36]. The results of the present study are in agreement with the prior literature.

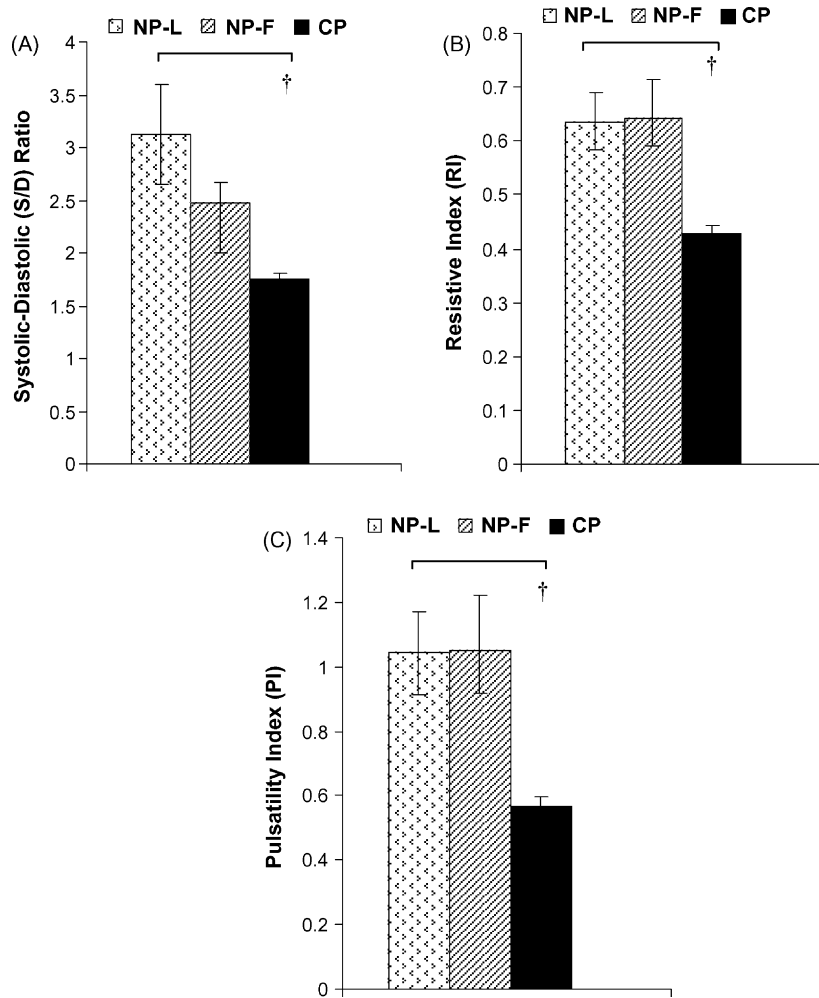
#### 4.2. Hemodynamic measurements and analyses

$P_{\text{Mean}}$  and HR have been reported not to change with the ovarian cycle [15,37–39], as found herein. In late gestation pregnant sheep, however,  $P_{\text{Mean}}$  and HR have been found to decrease [10–12,15,16,34]. Our measurements of  $P_{\text{Mean}}$  and HR did not decrease with pregnancy and indeed were elevated from those measured previously in unanesthetized, standing (non-supine position) [10–12,15,16,34]. Additional studies by our group suggest that these differences are due to the combined effects of posture (supine vs. standing) and anesthesia (data not shown).

The 2-fold decrease in UVR from the luteal phase (NP-L) to the follicular phase (NP-F) is most likely related to estrogen-mediated vasodilation. As noted above, we found that the ratio of E2 to P4 increased during the follicular phase; in prior work, the ratio of E2 to P4 has been shown to cause vasodilation, especially in the uterine vascular bed [2,9–11,16,40–42]. The likely mechanism by which increases in E2:P4 decrease resistance is via increased production of the potent endogenous vasodilator nitric oxide. Prior data from our group have shown that vasodilation *in vivo* is initiated by a rise in nitric oxide production that is mediated by endothelial estrogen receptors [2,15]. In CP animals, the E2:P4 was equivalent to luteal phase levels whereas UVR was nearly 20-fold lower. Thus, E2:P4 was not a predictor of UVR despite the similar E2:P4 values. In pregnancy, it is well known that resistance-sized arteries are transformed into the uteroplacental bed [21,41,43,44], which is largely independent of E2:P4 during late gestation. This uterine vascular transformation is likely the dominant mechanism by which UVR decreases with pregnancy.

Vascular impedance measurements enable the characteristics of more proximal (to point-of-measure) arteries to be distinguished from those of more distal vessels. In addition, impedance offers a more complete description of the hemodynamic work required to perfuse a vascular bed than the more commonly used resistance. One disadvantage of impedance is that the full frequency-dependent magnitude and phase spectra are required for a complete understanding of pressure–flow relationships. However, if one is only interested in large artery size and stiffness and wave reflections at the vascular bed origin, metrics of impedance based only on the magnitude can be useful. Herein we investigated the effects of the ovarian cycle and pregnancy on two metrics of impedance that give insight into large, conduit artery characteristics:  $Z_c$  and  $R_w$ .

Measurements of uterine vascular characteristic impedance changes during the ovarian cycle have not been previously reported. Characteristic impedance  $Z_c$  is directly proportional to proximal (to point-of-measure) arterial stiffness and inversely proportional to proximal arterial inner diameter. Stiffness, in turn, is proportional to elastic modulus and wall thickness and inversely related to inner diameter [45]. During the follicular phase,  $Z_c$  tended to decrease, although not significantly, which suggests a small increase in inner diameter since no change in elastic modulus was found (Fig. 5). In contrast, with pregnancy,  $Z_c$  decreased significantly (Fig. 3A), which is explained by the significant decrease in large artery elastic modulus (Fig. 5).



**Fig. 4.** Three indices of blood flow pulsatility used clinically, systolic-to-diastolic ratio (S/D), resistive index (RI), and pulsatility index (PI), computed for NP-L, NP-F and CP animals. No differences were seen in (A) S/D, (B) RI and (C) PI between NP-L and NP-F animals. In contrast, all three showed reductions with pregnancy compared to NP-L ( $p < 0.001$ ), which indicates decreased blood flow pulsatility. Data are means  $\pm$  S.E.

Measurements of wave reflection at the entrance to the uterine vascular bed during the ovarian cycle also have not been previously reported. The index of wave reflection  $R_w$  reflects mismatch between proximal and distal (conduit and resistance, respectively) artery impedance. Here we found that  $R_w$  remained unchanged between the luteal and follicular phases of the ovarian cycle (Fig. 3B). This is an interesting finding given the statistically significant decrease in downstream resistance. That is, the small but not significant decrease in  $Z_c$  coupled with the significant decrease in UVR (and thus  $Z_0$ ) was sufficient to normalize  $R_w$ . This finding suggests that small increases in conduit artery inner diameter maintain pulse wave reflection at a constant level during the ovarian cycle.

**Table 2**

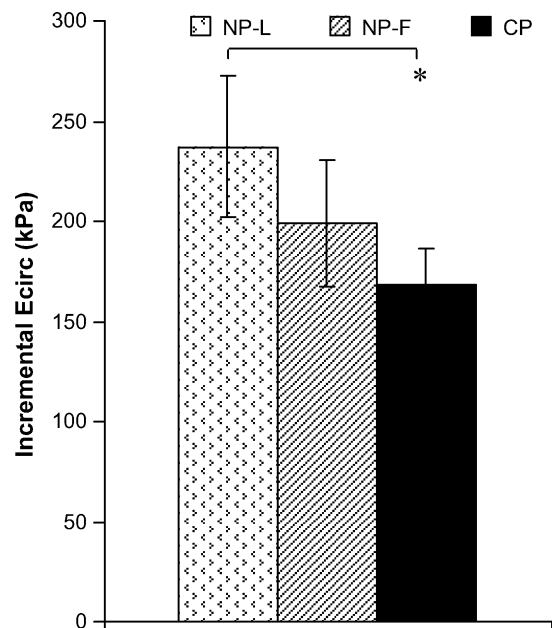
Inner diameter, outer diameter and wall thickness measured from secondary uterine arteries fixed at *in vivo* pressures ( $ID_f$ ,  $OD_f$  and  $WT_f$ , respectively). With pregnancy, ID and OD were increased compared to NP-L and NP-F groups.

	$ID_f$ (mm)	$OD_f$ (mm)	$WT_f$ (mm)
NP-L	$1.27 \pm 0.21$	$1.94 \pm 0.24$	$0.34 \pm 0.04$
NP-F	$1.58 \pm 0.12$	$2.50 \pm 0.09$	$0.42 \pm 0.06$
CP	$3.37 \pm 0.15^{\ddagger, \dagger}$	$3.99 \pm 0.22^{\ddagger, \dagger}$	$0.33 \pm 0.02$

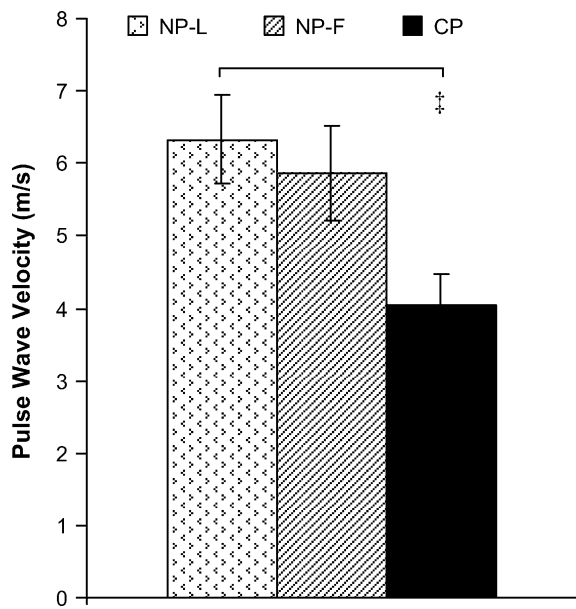
Data are means  $\pm$  S.E.

$\dagger$  Indicates significant difference between CP and NP-F ( $p < 0.001$ ).

$\ddagger$  Indicates significant difference between CP and NP-L ( $p < 0.00001$ ).



**Fig. 5.** Circumferential elastic modulus of large uterine arteries from NP-L, NP-F and CP animals.  $E_{circ}$  did not change with the ovarian cycle (NP-L vs. NP-F) but was decreased in CP animals compared to NP-L animals ( $*p < 0.05$ ). Data are means  $\pm$  S.E.



**Fig. 6.** Pulse wave velocity (PWV) within large uterine arteries calculated from uterine artery circumferential elastic modulus and diameter for NP-L, NP-F and CP animals. No differences were observed between NP-L and NP-F animals. PWV decreased with pregnancy ( $p < 0.001$ ). Data are means  $\pm$  S.E.

It is noteworthy that wave reflection during pregnancy was almost zero. The spiral arteries in women and terminal caruncular-placentomal arteries in sheep are intrinsically transformed into the uteroplacental bed with pregnancy [21,41,43,44,46]. Since the muscular integrity of these arteries essentially disappears with pregnancy, and since wave reflections also nearly disappear with pregnancy, these arteries are likely a significant source of wave reflections in the nonpregnant uterus.

Clinically, the pulsatility of uterine blood flow is characterized via non-invasive measurements of instantaneous systolic and diastolic flow. Blood flow indices, including S/D, RI and PI, are able to detect reactivity to vasodilators [47–49] and improper uterine perfusion associated with preeclampsia when used in combination with other features of the blood flow waveform [50–53]. However, changes in clinically used uterine blood flow indices during the ovarian cycle in sheep have not been previously reported. Some differences between the ovarian cycle of humans and sheep are important to consider here. The ovine ovarian cycle is approximately 15–17 days, with a relatively short (48–56 h) follicular phase, the latter being periovulatory. In women, a longer follicular phase (~10–14 days), including a menstrual period at its beginning, extends the human ovarian cycle to approximately 28–30 days. During this prolonged follicular phase in humans, estrogen levels rise slowly, reaching very high levels close to ovulation, and then fall. The follicular phase in humans is largely a time of rising (but still lower than in the luteal phase) ovarian E2 production, because unlike the ovine model the human corpus luteum produces significant levels of estrogen. Because of this difference in ovine ovarian versus human menstrual cycle, it maybe more correct to compare clinical blood flow index results in the follicular phase in ewes to the late-follicular stage of the human just around the time of ovulation.

From the early- or mid-follicular to luteal phase in women, uterine blood flow increases and RI and PI decrease [54,55]. In our studies in sheep, no changes in S/D, RI or PI were observed between NP-L and NP-F. We suggest that the lack of change in these indices in ewes is due to the shorter follicular phase compared to the human. The significant decreases in S/D, RI and PI in pregnant

sheep are consistent with the literature in humans [19,50,56,57] and suggest significant decreases in blood flow pulsations.

#### 4.3. Uterine artery mechanical measurements and analyses

Uterine artery outer diameter, wall thickness and circumferential incremental elastic modulus did not vary over the ovarian cycle. It is important to note that these measurements were made in arteries with no smooth muscle cell tone. Certainly changes in tone over the ovarian cycle, possibly mediated by estrogen and the E2:P4 ratio, could alter large uterine artery diameter, wall thickness and elastic modulus. However, expected consequences of the possible changes in structure and function were not evident in the uterine vascular impedance measurements discussed above. Thus, we expect that the impact of the ovarian cycle on smooth muscle cell tone in large uterine arteries is minimal. Another limitation of these results is that they may have limited applicability to other species, such as the human, with longer follicular phases; i.e. the 48-h follicular periovulatory phase of the sheep may be too short for changes in structure and function to occur other than by changes in smooth muscle cell tone.

The 2-fold increase in OD and 2-fold decrease in  $E_{\text{circ}}$  with pregnancy are in agreement with studies in other species [20–22,24]. There exists in the literature only one study using the sheep model to investigate the effects of pregnancy on the mechanics of large uterine arteries [25]. In contrast to the data in all other species and the results we report herein, Griendling et al. found that uterine artery elastic modulus increased with pregnancy [25]. However, it is important to note a methodological difference. We calculated elastic modulus as the slope of the stress–strain relationship in a physiological pressure range, whereas Griendling et al. calculated an incremental elastic modulus as a function of pressure [25]. These different methods can lead to different conclusions especially under conditions of large strain (approaching 100%). In terms of interpretation, both our data and the data by Griendling et al. show that the pregnant arteries have a larger change in diameter for an increment in pressure than the nonpregnant arteries. Thus, the pregnant arteries are less stiff.

Clinical studies have measured wave speed in systemic arteries over the human menstrual cycle and did not report any changes [38,39]. For example, Hayashi et al. found that PWV in the carotid-to-femoral artery was 5.4 m/s (S.D. 0.6) in the follicular phase and also 5.5 (S.D. 0.8) in the luteal phase [38,39]. Ounis-Skali found higher velocities in the femoral artery but still no differences over the ovarian cycle (8.13 S.D. 0.91 m/s vs. 7.85 S.D. 0.79 m/s for follicular vs. luteal) [40]. The PWVs found here in the uterine artery were in this same range in the follicular and luteal phases and also did not vary between over the ovarian cycle. However, we note that smooth muscle cell tone could vary over the ovarian cycle and alter PWV. All measurements on which the PWV calculation is based were made in the absence of smooth muscle cell tone. With pregnancy, the increase in OD and decrease in  $E_{\text{circ}}$  resulted in a dramatically decreased PWV, to about 4 m/s. The combination of decreased pulse wave velocity and decreased wave reflections with pregnancy emphasizes the increased conduit function of the uterine vasculature during pregnancy. That is, these data suggest that the proximal and distal vasculature remodel and transform, respectively, during pregnancy to allow maximally increased blood flow to the fetus.

In summary, uterine vascular impedance is a useful measurement with which the effects of physiological or pathological changes in the uterine vasculature can be investigated. The combination of impedance and arterial mechanics data presented here strongly supports the effect of changes in the E2:P4 ratio during ovarian cycle on the uterine resistance arteries but not uterine conduit arteries. With pregnancy, both resistance and

conduit arteries are significantly altered and these structural and functional changes in the vasculature affect uterine vascular pressure–flow relationships. Finally, our data suggest that impedance metrics are more sensitive to changes in uterine vascular structure and function than clinically used blood flow indices and may be diagnostically useful.

### Condensation

Ovine uterine vascular impedance measurements demonstrate that pregnancy causes large and small artery dilation and remodeling whereas the ovarian cycle causes only small artery dilation.

### Conflict of interest

None declared.

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